

Leaching of Lead and Other Elements from Portable Electronics, Part II

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Abstract

Portable electronic device circuit packs were ground up to more than meet EPA sieving criteria and were then subjected to the well known EPA Method 1311 leaching protocol. Based on work from the previous study, mainly Fe, Ni, Cu, Zn, and Pb were investigated. Leachate was also separately treated with egg whites and cardboard and the dissolved metal concentrations were found to be significantly reduced. Individual spikes of 500mg Fe, Ni, Cu, Zn, and Pb (artificial leachate) were run through columns of topsoil, sand, gravel, vermiculite and perlite to compare to the earlier work using topsoil, in a continuing effort to show what might happen if leachate were to escape from a landfill.

Introduction

Our previous work¹ dealt with looking at grinding efficiencies for printed circuit packs (PCBs), the analysis of the TCLP leachates, the effect of carbonate and sulfide and the capacity of topsoil to take up such leachates. One portion of the present work looks at two representative materials that would be in municipal solid waste (MSW) and their effect of heavy metal laden leachate. The materials chosen were eggs, specifically the whites, and cardboard. These materials were not chosen at random. Paper products make up 40 - 50% of the waste stream² and although the amount of cardboard is being reduced as more and more is being recycled, it nevertheless still makes up a large proportion of MSW, even more so on a volume or surface area basis.

Although the proportion of eggs in a land fill would be vanishingly small on a percentage basis, some will be there as a result of portions sticking to egg shells, eggs thrown out because they were rotten, some accidentally broken and portions scraped from plates into the garbage. And like cardboard eggs also have a reasonably high level of sulfur content³. Previously it was shown that sulfide has a significant effect on the solubility of the heavy metals extracted by the EPA leachate.

Sand and gravel are other materials surely to be found around some landfills, so they were chosen as “soil” materials to examine for their ion exchange capacity. Vermiculite and perlite were chosen more for interest. As purchased by the consumer, both of these materials are not in their natural form. Perlite⁴ is an artificially created frothy glass, similar to natural pumice. The flash evaporation of the water in the rock known as pearlstone is heated to its softening point (1500 – 200C) results in a light, porous material with a large surface area. Its low density makes it ideal as a filler in plasters and concretes and for use by the home gardener. Vermiculite⁵ in its raw form is a hydrated magnesium aluminosilicate which is exfoliated by heating before been sold for retail purchase. Its ion exchange ability is retarded by removing the waters of hydration. This work will show how much ability it still has to hold metal ions from artificial leachate.

This paper again uses the EPA Method 1311, Toxicity Characteristic Leaching Procedure (TCLP)⁶ as the testing basis for the leaching studies. This is the most common form of leaching test currently used in North America. Several individuals have expressed concern about this test^{7, 8}. The reason for this lies in the extreme solubility of lead acetate, as opposed to more common salts of lead. See Table 1⁹⁻¹¹. Note that this table corrects some unusual values listed in the equivalent table of reference one. It is important to keep in mind that this test is to determine the absolute worst case for leachate formation, NOT to determine what actually leaves the landfill as leachate. The concern that has been raised about this test is that this very important distinction is not always made, especially by those that read report data and have no chemical background.

In the present work the protocols called out in the EPA method have been adhered to for the testing. However, the samples for this study were ground to small particles and powders.

The samples in this study were analysed for the following elements: silver, barium, copper, iron, nickel, zinc and lead. The latter five were the individual elements found to have the highest concentrations in the previous study. Lead was an obvious choice, as this element and its compounds are singled out in the RoHS directive^{10, 11} to essentially be eliminated from electronics covered by the directive. For classes of electronics and specific cases where their use will at least be allowed for a while, see the directive. The other elements are heavy metals of varying concern.

Silver and copper was chosen for two reasons – they are principle elements in the new Pb-free solders, commonly referred to as SAC alloys and there is also enough economic worth in printed circuit assemblies (PCAs) to consider their recovery. Zinc is included in some specific Pb-free solders. Iron and nickel are common materials in lead frame materials and nickel is of course used in ENIG surface finishes. Some concern has been expressed over nickel and barium.

Table 1 - Solubility of Some Lead Salts

(Superscripts are degrees Celsius)

		g/100 ml	mg/L
•	Lead acetate	221⁵⁰	2,210,000
•	44.3²⁰		
•	443,000		
•	Lead chloride	1.08²⁵	10,800
•	Lead sulfate	0.0044²⁵	44
•	Lead hydroxide	0.00012²⁰	1.2
•	Lead carbonate	0.0001	1
•	Lead phosphate	0.000014²⁵	0.14
•	Lead sulfide	“insoluble”	

Experimental

Samples used for this study were taken from whole portable electronic units, different models from the previous study, but of the same general type and concentration of metals. They were soldered with Sn36Pb2Ag solder. The plastic casings, the LCD modules and RF shields were not subjected to testing.

As already mentioned in the Introduction, the analytical protocol used is EPA method 1311, TCLP. Samples were cut to EPA specified size using a cross-sectioning cut-off saw. As per 1311 instructions, initial work showed that extraction fluid # 1 was necessary (acetic acid/NaOH/ASTM Type II water).

The grinding in this study was performed with an IKA M20 universal grinder with a tungsten carbide blade. The grinding time was 20 minutes. The ground boards were then sieved through a 9.5 mm (3/8 in.) mesh sieve (as per 1311) and then were also sieved using 500 µm (#35), and 180 µm (#80) sieves. The portions that fell through the #35 mesh were combined and used for this study.

Each sample plus the requisite amount of EPA leaching solution were put in unused, clean plastic bottles. These were carefully closed with Teflon tape being used on the bottle threads. The bottles were then clamped and taped into a tumbler¹² capable of holding up to 12 bottles simultaneously. The tumbler mixed the samples end-over-end at 30 rpm for 18 hours as per the EPA method.

Each of the treated leachate portions were then filtered using the EPA required filter matt and then each portion was divided into 4 parts.

The first part of the leachate for each board was analyzed using ICP.

Twenty grams of egg white was added to an additional 40 ml part of the leachate for each board and was mixed for 5 min in a blade mixer. This mixture was then divided into two parts. The first part was filtered through a TCLP glass fiber filter (0.7 µm) and the extract was analyzed by ICP. The second part of the mixture was centrifuged for 15 min using an International Equipment Company; Model CL centrifuge run at a setting of 5000 rpm and the extract was analyzed by ICP.

Twenty grams of cardboard was added to another 40 ml part of the leachate for each board and was mixed for 5 min in a blade mixer. This mixture was then divided into two parts. The first part was, as above, filtered through a TCLP glass fiber filter (0.7 µm) and the extract was analyzed by ICP. The second part of the mixture was centrifuged for 15 min and the extract was analyzed by ICP.

The fourth part of the leachate for each board was itself used like a leaching solution for leaching soil. The soil: leachate proportion of 1:20 was used for each board and was tumbler mixed for 18 hours (according to EPA method). The “Method blank” was EPA leaching solution #1 mixed with soil in the same proportion 1:20. Then, each leachate was filtered using the EPA required filter matt and analyzed by ICP.

A separate set of experiments was also conducted. Twenty chromatographic columns were prepared using topsoil, gravel, sand, vermiculite and perlite four for each soil type. All of the twenty columns were then each spiked with 500ug of the elements Fe, Ag, Cu, Ba, Zn, Ni and Pb in 5 ml of 2% HNO₃.

Seven separate portions of 20 ml of Milli-Q water were percolated through each of the first set of ten columns, two columns for each soil type. Each portion of the eluant was collected and analyzed separately by ICP. For the second set of ten columns, seven 20ml portions of EPA leaching solution #1 were used for each column instead. Every 20 ml portion of the eluants collected was also analyzed separately by ICP.

Analysis for the metals was conducted with a Perkin Elmer Optima 3000 DV ICP-OES unit (Inductively Coupled Plasma – Optical Emission Spectrometer). The ICP-OES was calibrated for each element and calibrations were checked by verification standards for quality control purposes. Recovery of the verification standard for each element was between 90% and 110%. Method Detection Limits are shown in Table 2.

Table 2- Metal Analysis Method Detection Limits for Optima 3000 DV ICP

Element	MDL (ppm)
Silver (Ag)	0.003
Copper (Cu)	0.004
Iron (Fe)	0.002
Nickel (Ni)	0.003
Lead (Pb)	0.007
Zinc (Zn)	0.002
Barium (Ba)	NA

Results and Discussion

First part of the circuit board leachate

Two PCBAs from different but identical units were ground up as described in the experimental section. The results are shown in Figure 1 and Table 3. As can be seen, the agreement in the results between the two PCAs is quite good. Only for the iron results and for the copper results for material through the #80 mesh screen are the results different by more than 2 ppm.

When comparing the results for the material captured by the screens and what went through, only nickel has values that are even of the same order of magnitude. Iron, the hardest of the elements measured, was the only one retained more on the screens than passed through.

A comparison of the materials that went through the #80 mesh from the last study and from this study is shown in Table 4 and Figure 2. The data from the previous study is the average for three samples, including one where there was a different color to the solution due to a higher concentration of copper from the other two. The average values from this study are for the results tabulated in Figure 3 for the two boards used. The agreement is actually again quite good; when one considers that different models of devices were used in the two studies.

Table 3 - ICP Analysis Results for Materials from PCBAs Leached by EPA Method 1311

(all values in mg/L)	Ba	Cu	Fe	Ni	Zn	Pb
Board #1 On #35 + on #80 (mg/L)	7.74	0.3	592	17.6	0.66	2.64
Board #2 On #35 + on #80 (mg/L)	7.19	0.3	525	17.9	0.47	3.06
Board #1 Through #80 mesh (mg/L)	31.2	470	7	39.2	34.4	490
Board #2 Through #80 mesh (mg/L)	32.5	452	1.86	39.6	34.4	492

Table 4 - Comparison of Previous and Current Results for Leaching of Pulverized Handsets

	Previous study	Current study
Cu	360	461
Fe	51	4.43
Ni	22	39.4
Pb	258	491
Zn	23	34.4

Second and third parts of the circuit board leachate

Separate portions of 40 ml of the leachate of material through the #80 mesh were treated with either 20 grams of egg white or 20 grams of cardboard, mixed and then either filtered or centrifuged. The resulting solutions were analyzed by ICP. The results are shown in Figure 2 and Table 4.

The egg whites had essentially no effect on barium and nickel concentrations, only a moderate effect on zinc, but rather dramatic results on the concentrations of iron, copper and lead. Except in the case of iron, the results were even more

dramatic with cardboard. Whether this is due to poorer affinity for iron or additional iron coming from the cardboard is not known, as the cardboard was not tested itself for leachate potential.

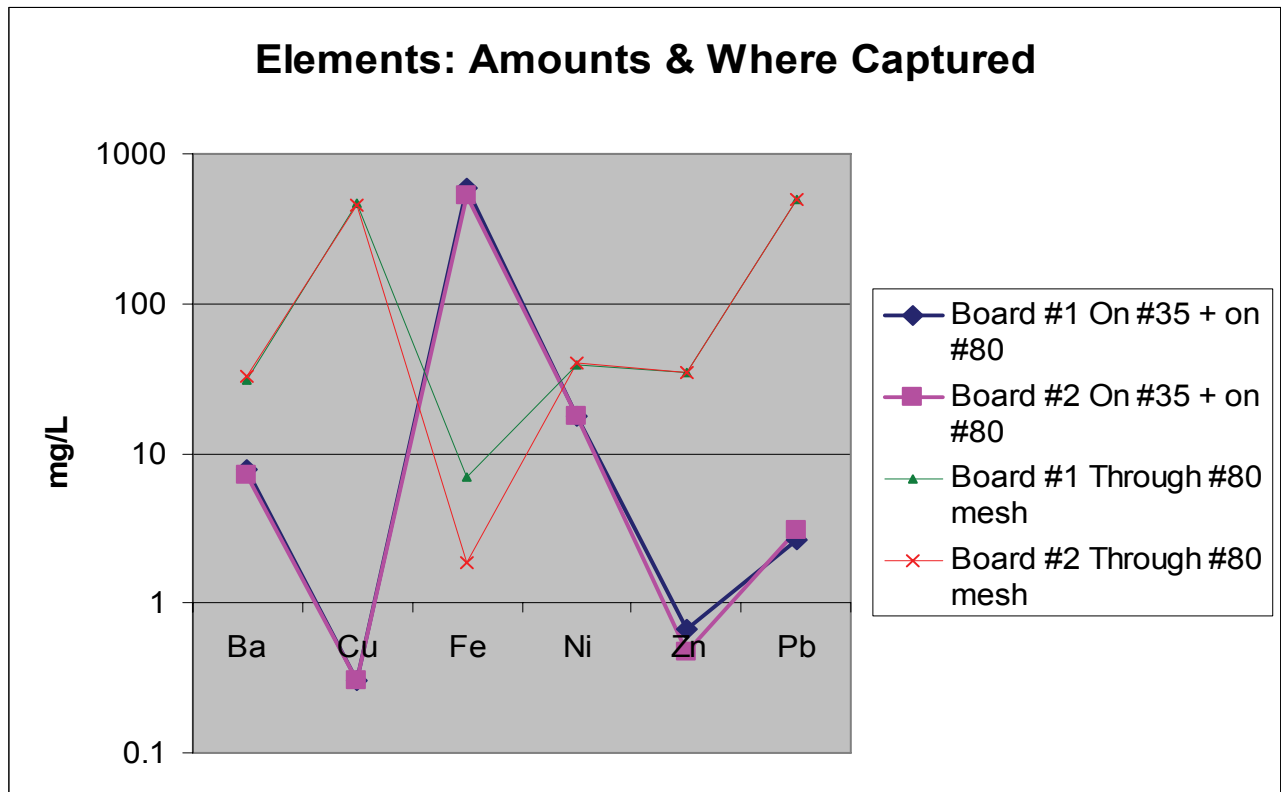


Figure 1 - EPA Method 1311 Leaching Results for Two Ground Printed Circuit Packs

Table 4 - Effect of Egg Whites or Cardboard on Concentrations of Heavy Metals

	Ba	Cu	Fe	Ni	Zn	Pb
Average Through #80 Mesh (mg/L)	31.85	461	4.43	39.4	34.4	491
Average Through #80 Mesh + Egg Whites (mg/L)	32.25	60.6	0.034	37	23	17.6
Average Through #80 Mesh + Cardboard (mg/L)	12.3	28.75	0.145	16.05	10.06	2.365

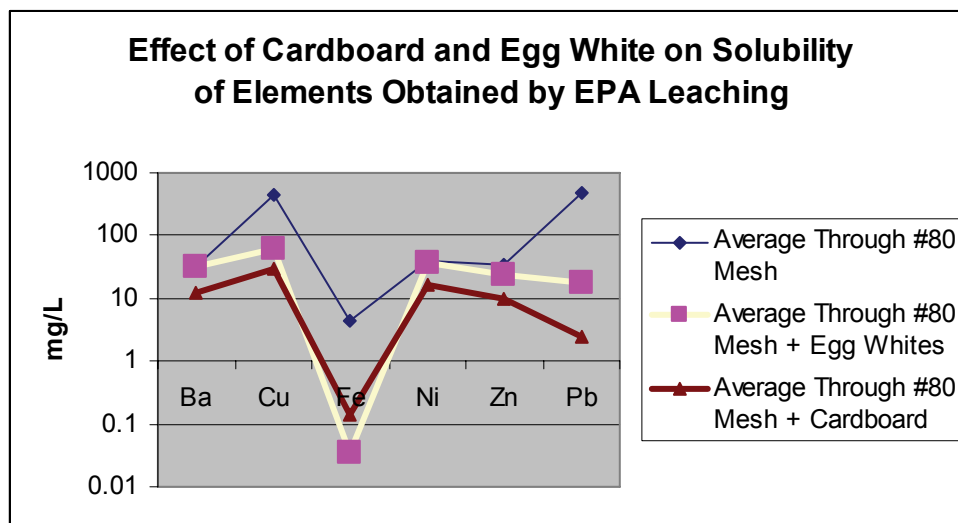


Figure 2 - Effect of Common Landfill Materials on Heavy Metal Leachate Solubility

Fourth part of the circuit board leachate

This portion of the investigation dealt with the extent of how tightly heavy metals are bound to topsoil. After leaching the two different separated sizes of ground particles from the two circuit boards, collecting the leachates and filtering, they were then mixed in the 1:20 portion with topsoil, tumbled, filtered and then reanalyzed. The results below in Table 5 and Figure 3 show very good agreement between the results for the two boards. The values show that the topsoil has a dramatic effect upon the amount of heavy metals in solution. The following show the approximate values in mg/l for the ionic concentrations before and after mixing with topsoil: (Ba – 32 -> 6), (Cu – 461 -> 12), (Fe – 4.4 -> 0.03), (Ni – 39.4 -> 6.0), (Zn – 34.4 -> 8.7) and (Pb – 491 -> 9). These correspond to the following decreases in concentrations: Ba 6x, Cu 38x, Fe 147x, Ni 7x, Zn 4x and Pb 61x. These are quite large decreases in concentrations.

Table 5 - Results of a 1:20 Mixture of Topsoil:EPA Leachate

	Ba	Cu	Fe	Ni	Zn	Pb
#1 On #35 + on #80 + Soil (mg/L)	1.42	0.332	0.674	0.861	0.742	0.177
#1 Through #80 mesh + Soil (mg/L)	5.66	11.50	0.030	5.980	8.540	8.100
#2 On #35 + on #80 + Soil (mg/L)	1.36	0.323	0.548	0.892	0.762	0.095
#2 Through #80 mesh + Soil (mg/L)	6.03	11.90	0.027	6.100	8.850	9.560

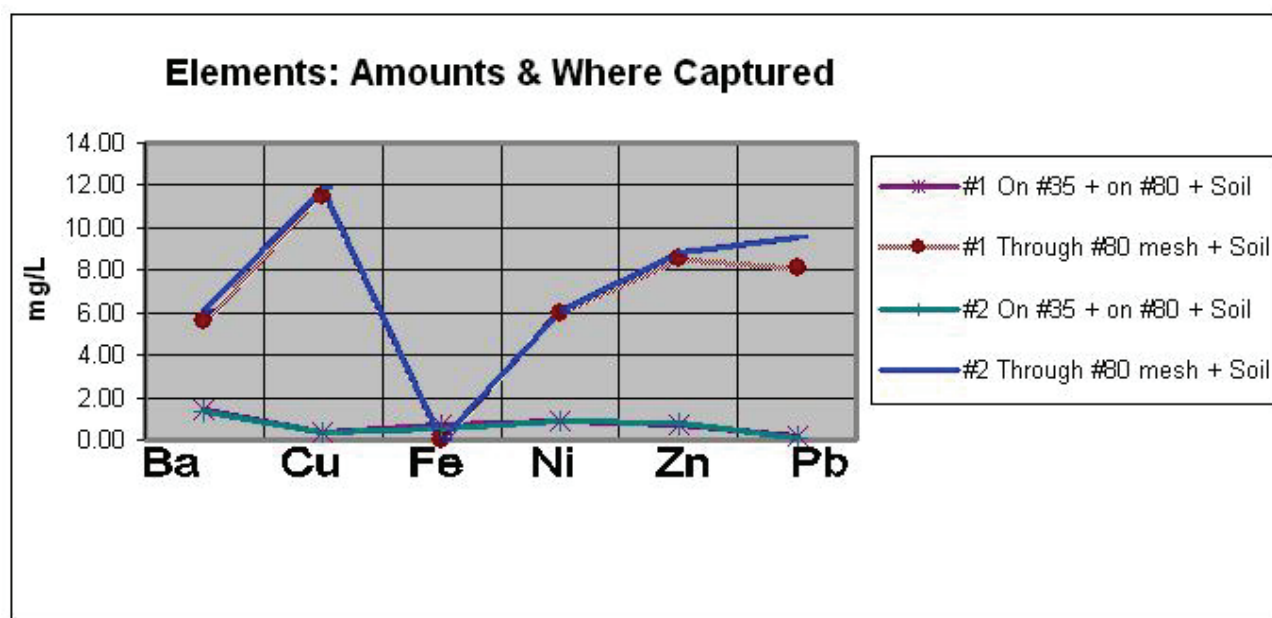


Figure 3 - Leachate mixed with topsoil in a Leachate:Topsoil ratio of 20:1, mixed, filtered and analyzed

Last part of the investigation

This portion of the study deals with the capability of columns of “soils” to take up elements from artificial leachate and keep it.

A solution of soluble salts of barium, silver, copper, iron, nickel, zinc and lead was made up. Five milliliter spikes containing 500 ug of each metal ion were each put on columns with different “soils”. The columns were packed with either: 5 grams of topsoil; 10grams of sand; 10grams of vermiculite; 10grams of perlite or 145grams of gravel. Ideally the same mass or same surface area of material would have been used in each case. However, this was not possible due to not knowing the surface area of the materials and the differing abilities of the materials to hold the salt solutions. The extremes of essentially no porosity and channeling had to be avoided. This could only be done by using less topsoil and a significantly larger amount of gravel.

Seven 20 ml portions of deionized water were then run through two columns of each type of material. The resulting seven twenty milliliter aliquots for each column were collected and analyzed separately to determine the amount of the heavy metals from the artificial leachate not held by the topsoil, sand, gravel, vermiculite and perlite. This was repeated for the other set of columns with the same “soils” and same size of metal spiked solutions added, but the EPA 1311 leaching solution was used instead of deionized water for running through the columns. This was done to determine the differing abilities of these two liquids (DI water and EPA solution) to retrieve metals from soil. The detailed spreadsheets for topsoil and the other “soil” materials are given in the APPENDIX. See Figures 4 – 8 for graphical representations of the results.

The tables of data show that in many cases the blanks gave significant amounts of the ions of interest coming from the columns. The blank values were subtracted from the values obtained for the spiked columns. In the cases where negative values were obtained, zero values were entered in the accompanying graphs.

Topsoil

For the DI water leaching of topsoil, only nickel recovery was bigger than the blank values. It would appear that the presence of the materials in the spike was actually retarding the DI water from leaching more material from the column of topsoil. Even ignoring the blank, the total amount of zinc, lead and silver removed from the soil in both cases was less than 0.7 ppm per element. Only very small portions of zinc and lead were leached with the first 20 ml portion of DI water and then no more was detected during analysis. It is quite possible that the lead and zinc detected was a small portion of these ions that had never been taken up by the soil, but had remained in solution and so was easily swept out by the first aliquot. The values for copper and nickel were also small, 4 and 2 ppm, respectively. The most dramatic change in the amount leached over the course adding the seven aliquots of DI water was for barium, where after the first two 20 ml leaches with DI water the amount coming off the soil was reduced to essentially 0.01 mg/L. The results for the two separate columns were in good agreement, within 1 ppm of each other.

As expected, leaching with the EPA solution resulted in more materials being taken out of the topsoil. The blank values are also bigger, except for nickel. It is also noted that the agreement between the two columns run was actually quite poor. One column had most values in the single and double digit range while for the other one the values were double and triple digit. The definitive reason for this is known. Perhaps the topsoil from one column to the other was different or, more likely; the one with the larger values had channels in the material. Nevertheless, average values were plotted in Figure 4 for the EPA solution leach. Only iron again had a huge blank reading, with very significant amounts of barium, copper, nickel and zinc being recovered.

Other “soils”

Although all the other graphs exhibit the same general shape for the EPA leaching solution curves as seen in the topsoil graph, the amount of recovered heavy metals is much higher than for topsoil. Not surprisingly the sand holds the least, with the perlite, gravel and vermiculite showing about 80% recovery, except for the iron. Taking into account the blank, generally speaking the iron is the most tightly held by the different soils, with essentially little recovery from topsoil, sand or gravel when the soils are leached with the EPA solution or DI water.

Sand and gravel behave similarly whether the leaching medium is DI water or the EPA solution. This is not too surprising, as both materials are generally not considered very reactive. The reproducibility of results for sand was quite good, with the largest difference between the two columns being 26 ppm for zinc leached with DI. This represents a ~6% difference. Similar agreement was found for the two columns of gravel.

There are a few instances for perlite and gravel where DI water is apparently more aggressive in removing the metal ions. However, whether a 20% difference is real or is just the result of the natural variation of the system due to channeling, etc. is difficult to say. However, in the cases of lead leaching from sand, vermiculite and perlite where the difference is 40% or greater, it is likely that this is a real difference and the EPA solution is more aggressive, as expected.

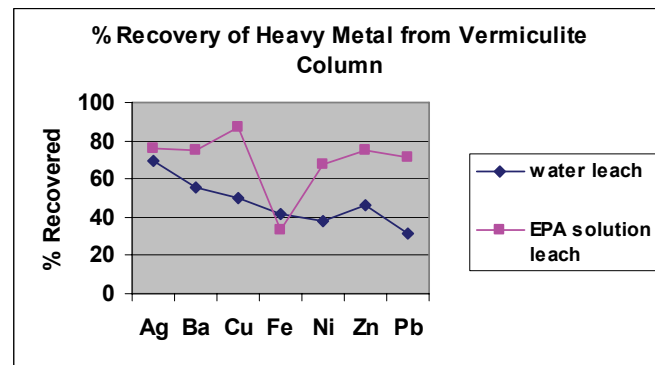
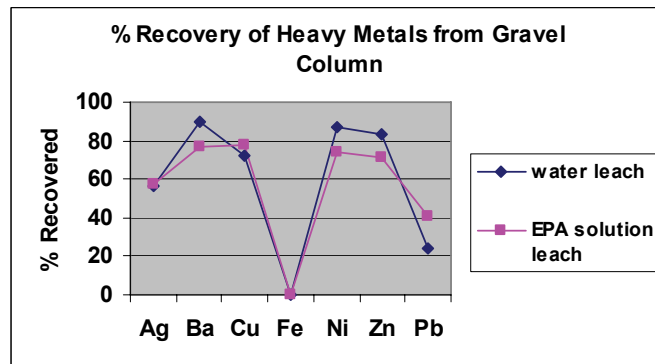
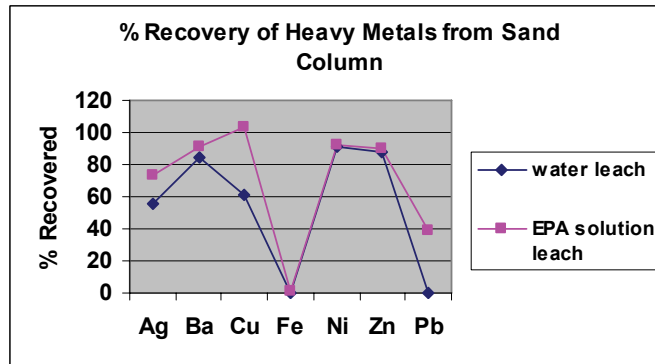
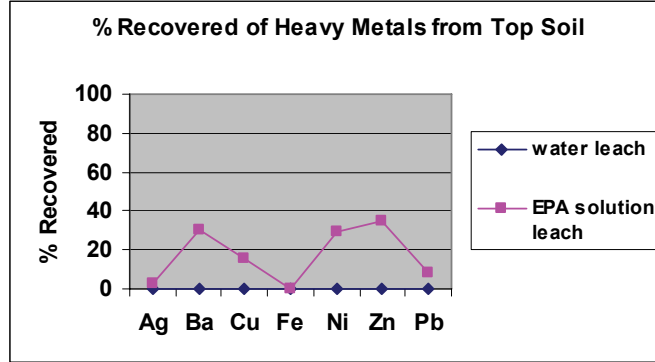
Raw vermiculite that has not been heated is known to have considerable ion exchange ability, especially in the presence of carboxylic acids¹³. However, once the vermiculite has been industrially heated and the waters of hydration are gone, the structure is more “fixed”. This would account for the relatively poor ability of the vermiculite to hold the metal ions.

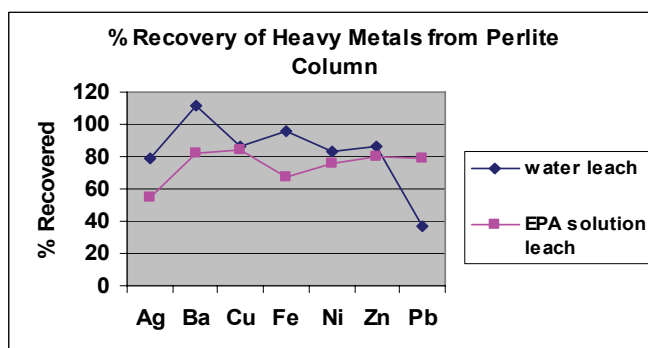
Conclusions

The present work has shown that there are several materials that could slow down if not stop the escape of heavy metals from a landfill. Any sulfur containing material will either have free sulfide or produce it during decomposition, resulting in one of the most potent precipitators of lead. Since landfills contain an abundance of paper, even with recycling, it is not likely lead will be escaping from any landfills soon.

Even if it does escape from a landfill, the analytical work completed shows that any heavy metals that leach into topsoil is not going anywhere, as the topsoil is extremely effective in sequestering lead and other metals. However, sand and gravel, which are more likely to be found lower down in the ground surrounding a landfill, are less able to hold the heavy metals. But looking at lead only, one sees that for a DI water leach, which is reasonably aggressive because of the chemical driving force, that sand will still only release 0.06% of a 500 mg/5ml solution of lead. Gravel will release about 25%. It is highly unlikely that there would be a plume of 100 ppm dissolved lead leaving a landfill. The possibility of any significant amounts of lead leaving a modern landfill in the geologically near future is quite remote.

Figures 4 – 8% Recovery of Heavy Metals from Different Soil





The opinions expressed by the authors are those of the individuals concerned and do not necessarily represent or reflect those of Research In Motion Limited and/or its affiliated companies

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APPENDIX

Soil 5g

Extraction with water

mg/L	Ag	Ba	Cu	Fe	Ni	Zn	Pb
Blank1		1.32	0.032	0.57		0.021	0.08
Spike1.1		0.973	0.018	0.595		0.016	0.034
Spike2.1		0.957	0.02	0.51		0.017	0.025
Blank2		0.374	0.035	0.73			0.014
Spike1.2		0.13	0.046	0.842	0.027		
Spike2.2		0.188	0.048	0.842	0.032		
Blank3		0.028	0.047	1.2	0.011		
Spike1.3		0.016	0.04	0.764	0.02		
Spike2.3		0.02	0.043	0.798	0.023		
Blank4		0.021	0.043	1.05	0.01		
Spike1.4		0.014	0.034	0.643	0.017		
Spike2.4		0.015	0.034	0.633	0.018		
Blank5		0.016	0.036	0.851	0.009		
Spike1.5		0.011	0.027	0.515	0.012		
Spike2.5		0.012	0.032	0.522	0.014		
Blank6		0.012	0.026	0.625	0.006		
Spike1.6	0.002	0.008	0.019	0.359	0.01		
Spike2.6	0.02	0.008	0.02	0.367	0.011		
Blank7		0.013	0.027	0.675	0.009		
Spike1.7	0.004	0.01	0.02	0.434	0.015		
Spike2.7	0.003	0.011	0.023	0.432	0.014		

Blank(ug)	35.68	4.92	114.02	0.9	0.42	1.88	
Spike1(ug)	0.12	23.24	4.08	83.04	2.02	0.32	0.68
Spike2(ug)	0.46	24.22	4.4	82.08	2.24	0.34	0.5
Theoretically %	0.024	-2.488	-0.168	-6.196	0.224	-0.02	-0.24
Recovery of Spike	0.092	-2.292	-0.104	-6.388	0.268	-0.016	-0.276

Extract with leaching solution

mg/L	Ag	Ba	Cu	Fe	Ni	Zn	Pb
Blank1		1.89	0.028	0.451	0.011	0.028	0.037
Spike1.1		1.66	0.03	0.324	0.038	0.082	0.035
Spike2.1	0.46	16.4	7.47	10.6	13.5	16.3	4.15
Blank2		0.718	0.049	1.31	0.016	0.047	0.031
Spike1.2		0.681	0.121	2.09	0.061	0.128	0.03
Spike2.2	0.158	0.166	0.359	2.21	0.168	0.142	0.151
Blank3		0.198	0.123	6.75		0.034	0.019
Spike1.3		0.229	0.14	2.78	0.057	0.042	0.016
Spike2.3	0.117	0.146	0.155	0.91	0.098	0.104	0.065
Blank4		0.105	0.08	4.81		0.02	0.1
Spike1.4		0.166	0.131	2.86	0.056	0.04	0.009
Spike2.4	0.097	0.289	0.06	0.258	0.102	0.166	0.028
Blank5		0.085	0.061	3.93		0.017	0.009
Spike1.5		0.136	0.089	1.97	0.041	0.037	
Spike2.5	0.099	0.411	0.052	0.222	0.118	0.196	0.032
Blank6		0.087	0.068	4.57		0.018	0.008
Spike1.6		0.108	0.072	1.61	0.032	0.028	0.004
Spike2.6	0.089	0.41	0.047	0.207	0.113	0.186	0.031
Blank7		0.062	0.044	2.59		0.012	
Spike1.7	0.091	0.37	0.053	0.254	0.109	0.169	0.034
Spike2.7	0.092	0.371	0.052	0.254	0.108	0.169	0.034

Blank(ug)	62.9	9.06	488.22	0.54	3.52	4.08	
Spike1(ug)	1.84	67	12.72	237.76	7.88	9.68	2.56
Spike2(ug)	22.24	364.06	164.74	306.22	284.84	345.64	90.68
Theoretically %	0.368	0.82	0.732	-50.092	1.468	1.232	-0.304
Recovery of Spike	4.448	60.232	31.136	-36.4	56.86	68.424	17.32

Sand (10g)

Extract with water

mg/L	Ag	Ba	Cu	Fe	Ni	Zn	Pb
Blank1		1.13	0.016	0.231	0.056	0.157	0.032
Spike1.1	12.7	21.5	15.1	0.078	22.4	21.4	0.047
Spike2.1	12.7	22.1	15.4	0.174	22.9	22.7	0.049
Blank2		0.021	0.016	0.107	0.011	0.016	
Spike1.2	0.792	0.227	0.146	0.016	0.167	0.108	
Spike2.2	0.700	0.237	0.151	0.011	0.167	0.120	
Blank3				0.276			
Spike1.3	0.173	0.043		0.072			
Spike2.3	0.165	0.045		0.046			
Blank4				0.343			
Spike1.4	0.084	0.036		0.04			
Spike2.4	0.075	0.038		0.072			
Blank5				0.336			
Spike1.5	0.052	0.019		0.144			
Spike2.5	0.044	0.020		0.124			
Blank6				0.218			
Spike1.6	0.047	0.015		0.108			
Spike2.6	0.045	0.021		0.273			
Blank7				0.191			
Spike1.7	0.047	0.016		0.081			
Spike2.7	0.045	0.018		0.218			

Blank(ug)		23.02	0.64	34.04	1.34	3.46	0.64
Spike1(ug)	277.9	437.12	304.92	10.78	451.34	430.16	0.94
Spike2(ug)	275.48	449.58	311.02	12.9	461.34	456.4	0.98
Theoretical %	55.58	82.82	60.856	-4.652	90	85.34	0.06
Recovery of Spike	55.096	85.312	62.076	-4.228	92	90.588	0.068

Spike1(ug)	278	437	305	11	451	430	1
Spike2(ug)	275	450	311	13	461	456	1

Extract with leaching solution

mg/L	Ag	Ba	Cu	Fe	Ni	Zn	Pb
Blank1		1.23	0.068	0.275	0.049	0.238	0.031
Spike1.1	16.2	22.5	22.4	0.988	22.5	21.7	3.53
Spike2.1	15	21.7	21.4	0.4	22.3	21	2.67
Blank2		0.296	0.075	0.021	0.031	0.117	0.02
Spike1.2	1.74	1.53	2.08	0.03	0.425	0.792	2.47
Spike2.2	1.75	1.94	2.3	0.03	0.577	1.03	2.19
Blank3		0.201	0.063	0.027	0.022	0.088	0.014
Spike1.3	0.683	0.466	0.774	0.022	0.06	0.212	1.28
Spike2.3	0.756	0.493	0.788	0.034	0.054	0.23	1.32
Blank4		0.154	0.066	0.047	0.021	0.086	0.014
Spike1.4	0.204	0.249	0.49	0.027	0.044	0.138	0.925
Spike2.4	0.207	0.265	0.513	0.043	0.047	0.153	0.968
Blank5		0.141	0.074	0.073	0.023	0.084	0.011
Spike1.5	0.066	0.207	0.389	0.06	0.04	0.116	0.733
Spike2.5	0.056	0.189	0.373	0.077	0.037	0.12	0.762
Blank6		0.129	0.098	0.111	0.022	0.079	0.013
Spike1.6	0.015	0.165	0.302	0.091	0.035	0.099	0.597
Spike2.6	0.017	0.173	0.311	0.089	0.034	0.113	0.609
Blank7		0.097	0.068	0.3	0.018	0.067	0.016
Spike1.7	0.107	0.216	0.275	0.015	0.078	0.497	
Spike2.7	0.118	0.237	0.272	0.021	0.087	0.501	

Blank(ug)		44.96	10.24	17.08	3.72	15.18	0.119
Spike1(ug)	378.16	504.48	533.02	29.86	462.38	462.7	200.64
Spike2(ug)	355.72	497.56	518.44	18.9	466.63	462.66	189.1
Theoretical %	75.632	91.904	104.556	2.556	91.732	89.504	40.1042
Recovery of Spike	71.144	90.52	101.64	0.364	92.582	89.496	37.7962

Perlite (10g)

Extract with water

mg/L	Ag	Ba	Cu	Fe	Ni	Zn	Pb
Blank1		0.16	0.29	0.464	0.019	0.044	0.011
Spike1.1	7.85	11.3	10.8	11.1	10.3	10.7	10.8
Spike2.1	4.26	8.06	7.58	8.31	7.23	7.5	7.49
Blank2		0.225	0.025	1.33	0.028	0.028	0.008
Spike1.2	8.54	11.5	11	11.1	10.4	10.8	11.1
Spike2.2	11.5	15.6	14.4	14.9	13.8	14.2	15
Blank3		0.088	0.006	0.428	0.007	0.008	
Spike1.3	2.46	3.6	3.41	3.05	3.2	3.37	3.34
Spike2.3	2.54	3.43	3.14	2.66	3	3.15	3.21
Blank4		0.03		0.07	0.005		
Spike1.4	0.794	1.04	0.983	0.563	0.914	0.973	0.894
Spike2.4	0.726	0.907	0.837	0.425	0.789	0.837	0.762
Blank5		0.011		0.017	0.006		
Spike1.5	0.261	0.361	0.344	0.081	0.326	0.345	0.251
Spike2.5	0.262	0.366	0.339	0.086	0.325	0.345	0.252
Blank6		0.006		0.013			0.007
Spike1.6	0.082	0.139	0.142	0.021	0.137	0.144	0.07
Spike2.6	0.101	0.158	0.151	0.025	0.149	0.158	0.085
Blank7		0.003		0.006			
Spike1.7	0.042	0.064	0.07	0.01	0.072	0.075	0.026
Spike2.7	0.058	0.092	0.093	0.015	0.094	0.099	0.032

Blank(ug)	10.46	6.42	46.56	1.3	1.6	0.38	
Spike1(ug)	400.58	560.08	436	518.5	414	430	216
Spike2(ug)	388.94	572.26	439.6	527.92	420.6	434	149.8
Theoreticaly %	80.116	109.924	85.916	94.388	82.54	85.68	43.124
Recovery of Spike	77.788	112.36	86.636	96.272	83.86	86.48	29.884

Extract with leaching solution

mg/L	Ag	Ba	Cu	Fe	Ni	Zn	Pb
Blank1	0.005	0.219	0.035	0.565	0.014	0.052	0.012
Spike1.1	3.3	7.01	6.98	7.56	6.61	6.91	6.78
Spike2.1	3.63	8.28	8.1	9.06	7.78	8.11	8.03
Blank2	0.004	0.191	0.016	0.684	0.015	0.014	0.005
Spike1.2	6.11	10.2	10.4	8.77	9.29	9.65	9.6
Spike2.2	7.86	12.3	12.5	10.4	11.2	11.6	11.7
Blank3		0.06	0.011	0.054	0.012	0.005	
Spike1.3	1.69	2.75	2.81	1.36	2.51	2.65	2.47
Spike2.3	1.6	2.66	2.71	1.08	2.41	2.55	2.31
Blank4		0.026	0.009	0.025	0.013	0.004	
Spike1.4	1.09	0.894	0.925	0.499	0.792	0.848	0.812
Spike2.4	0.924	0.576	0.58	0.352	0.492	0.533	0.539
Blank5		0.016	0.009	0.022	0.012	0.003	
Spike1.5	0.706	0.345	0.348	0.28	0.292	0.313	0.326
Spike2.5	0.617	0.205	0.2	0.223	0.164	0.178	0.209
Blank6		0.012	0.009	0.018	0.009	0.003	
Spike1.6	0.395	0.152	0.152	0.197	0.121	0.13	0.153
Spike2.6	0.385	0.103	0.1	0.173	0.079	0.084	0.104
Blank7		0.01	0.007	0.012	0.01	0.002	
Spike1.7	0.311	0.106	0.103	0.17	0.081	0.087	0.11
Spike2.7	0.31	0.087	0.085	0.135	0.062	0.069	0.091

Blank(ug)	0.155	9.585	1.745	24.775	1.63	1.4	0.28
Spike1(ug)	255.54	394.09	399.46	338.92	360.87	377.21	371.12
Spike2(ug)	288.37	442.82	445	383.16	404.84	421.93	419.51
Theoreticaly %	51.077	76.901	79.543	62.829	71.848	75.162	74.168
Recovery of Spike	57.643	86.647	88.651	71.677	80.642	84.106	83.846

Vermiculite (10g)

Extract with water

mg/L	Ag	Ba	Cu	Fe	Ni	Zn	Pb
Blank1	0.021	0.994	0.09	4.78	0.039	0.078	0.012
Spike1.1	8.86	9.91	8.9	9.52	7.6	8.64	6.84
Spike2.1	5	7.77	5.84	9.38	4.24	5.3	3.29
Blank2	0.026	0.918	0.075	7.16	0.057	0.06	0.007
Spike1.2	5.25	5.16	4.12	9.82	3.05	3.8	2.47
Spike2.2	5.93	5.48	4	10.5	2.68	3.55	2.01
Blank3	0.007	0.296	0.024	2.64	0.014	0.017	0.003
Spike1.3	1.81	1.25	0.857	5.2	0.597	0.781	0.427
Spike2.3	2.36	1.19	0.838	3.15	0.555	0.772	0.392
Blank4		0.119	0.009	1.32	0.008	0.005	0.004
Spike1.4	0.976	0.434	0.268	2.71	0.182	0.249	0.132
Spike2.4	1.41	0.518	0.346	1.64	0.218	0.318	0.15
Blank5		0.06	0.007	0.931	0.007	0.002	
Spike1.5	0.577	0.191	0.11	1.56	0.072	0.102	0.055
Spike2.5	0.962	0.249	0.155	0.906	0.088	0.145	0.07
Blank6		0.029		0.649	0.005		
Spike1.6	0.319	0.085	0.045	0.981	0.029	0.041	0.024
Spike2.6	0.666	0.141	0.085	0.601	0.042	0.077	0.042
Blank7		0.026		0.851	0.005		0.005
Spike1.7	0.23	0.059	0.029	0.944	0.019	0.025	0.012
Spike2.7	0.402	0.076	0.042	0.413	0.021	0.038	0.02

Blank(ug)	1.08	48.84	4.1	366.62	2.7	3.24	0.62
Spike1(ug)	360.44	341.78	286.58	614.7	230.98	271.44	199.2
Spike2(ug)	334.6	308.48	226.12	531.8	156.88	201.7	119.48
Theoreticaly %	71.872	58.588	56.496	49.616	45.656	53.64	39.716
Recovery of Spike	66.704	51.928	44.404	33.036	30.836	39.692	23.772

Extract with leaching solution

mg/L	Ag	Ba	Cu	Fe	Ni	Zn	Pb
Blank1	0.002	0.779	0.078	4.06	0.016	0.098	0.014
Spike1.1	8.67	10.8	10.3	8.11	8.82	9.65	7.51
Spike2.1	8.87	11.2	10.5	8.33	8.8	9.91	7.52
Blank2		0.671	0.06	3.54	0.016	0.052	0.007
Spike1.2	4.62	4.62	5	6.45	3.19	3.77	3.31
Spike2.2	4.82	4.91	5.19	6.38	3.37	4	3.51
Blank3		0.48	0.049	2.02	0.015	0.033	0.003
Spike1.3	2.01	1.95	2.8	1.42	1.55	1.74	2.45
Spike2.3	2.08	2.03	2.88	1.63	1.63	1.84	2.63
Blank4		0.414	0.038	0.861	0.009	0.024	0.005
Spike1.4	1.32	1.42	1.63	0.956	1.13	1.22	1.67
Spike2.4	1.38	1.46	1.69	1.31	1.2	1.27	1.78
Blank5		0.377	0.032	0.651	0.007	0.02	
Spike1.5	0.904	1.17	1.04	2.15	0.901	0.917	1.21
Spike2.5	0.879	1.13	0.974	0.795	0.906	0.915	1.2
Blank6		0.349	0.028	0.591	0.005	0.017	0.002
Spike1.6	0.638	0.972	0.702	0.959	0.735	0.722	0.886
Spike2.6	0.638	0.945	0.696	0.834	0.743	0.719	0.889
Blank7		0.321	0.025	0.479	0.004	0.014	0.005
Spike1.7	0.461	0.809	0.487	0.774	0.588	0.559	0.667
Spike2.7	0.457	0.803	0.474	0.99	0.594	0.567	0.67

Blank(ug)	0.04	67.82	6.2	244.04	1.44	5.16	0.72
Spike1(ug)	372.46	434.82	439.18	416.38	338.28	371.56	354.06
Spike2(ug)	382.48	449.56	448.08	405.38	344.86	384.42	363.98
Theoreticaly %	74.484	73.4	86.596	34.468	67.368	73.28	70.668
Recovery of Spike	76.488	76.348	88.376	32.268	68.684	75.852	72.652

Gravel (145g)

Extract with water

mg/L	Ag	Ba	Cu	Fe	Ni	Zn	Pb
Blank1		0.533	0.08	5.46	0.053	0.117	0.055
Spike1.1	10.6	21	17.1	6.97	20.1	19.5	4.84
Spike2.1	9.9	21.6	16.6	6	20.3	19.9	3.63
Blank2		0.099	0.056	3.66	0.033	0.04	0.035
Spike1.2	1.12	1.23	0.622	1.21	1.19	0.969	0.259
Spike2.2	1.28	1.75	0.906	1.8	1.69	1.47	0.406
Blank3		0.046	0.037	2.66	0.025	0.027	0.029
Spike1.3	0.75	0.251	0.28	3.49	0.129	0.124	0.495
Spike2.3	0.709	0.228	0.174	1.59	0.126	0.106	0.246
Blank4		0.045	0.046	3.39	0.032	0.033	0.035
Spike1.4	0.725	0.196	0.46	7.51	0.078	0.112	0.962
Spike2.4	0.567	0.115	0.114	1.74	0.04	0.035	0.246
Blank5		0.05	0.056	4.09	0.03	0.041	0.034
Spike1.5	0.471	0.088	0.13	2.4	0.029	0.033	0.278
Spike2.5	0.622	0.095	0.188	3.34	0.023	0.041	0.486
Blank6		0.026	0.022	1.96	0.019	0.018	0.016
Spike1.6	0.353	0.056	0.093	0.096	0.016	0.022	0.204
Spike2.6	0.454	0.06	0.126	2.49	0.01	0.029	0.317
Blank7		0.018	0.015	1.46	0.012	0.011	0.019
Spike1.7	0.216	0.028	0.03	1.03			0.068
Spike2.7	0.343	0.046	0.104	2.16	0.011	0.025	0.261

Blank(ug)	0	16.34	6.24	453.6	4.08	5.74	4.46
Spike1(ug)	284.7	456.98	374.3	454.12	430.84	414.76	142.12
Spike2(ug)	277.5	477.88	364.24	382.4	444	431.04	111.84
Theoretic	56.94	88.128	73.612	0.104	85.352	81.804	27.532
aly %	55.5	92.308	71.6	-14.24	87.984	85.06	21.476

Extract with leaching solution

mg/L	Ag	Ba	Cu	Fe	Ni	Zn	Pb
Blank1		0.82	0.129	5.84	0.044	0.229	0.061
Spike1.1	10.9	17.3	16.9	11.4	16.8	16.1	7.23
Spike2.1	9.58	18.4	16.8	6.09	17.9	17	5.21
Blank2		0.309	0.065	4.17	0.028	0.069	0.036
Spike1.2	1.56	1.87	1.67	3.55	1.32	1.24	1.5
Spike2.2	1.01	1.57	1.51	2.41	0.893	0.949	1.38
Blank3		0.204	0.044	2.54	0.019	0.05	0.026
Spike1.3	0.8	0.504	0.507	1.49	0.149	0.252	0.695
Spike2.3	0.672	0.533	0.563	0.858	0.137	0.267	0.768
Blank4		0.158	0.036	2.39	0.019	0.045	0.022
Spike1.4	0.684	0.306	0.333	1.25	0.057	0.152	0.531
Spike2.4	0.699	0.33	0.417	2.16	0.063	0.172	0.735
Blank5		0.137	0.151	2.07	0.018	0.04	0.018
Spike1.5	0.559	0.204	0.226	0.936	0.03	0.106	0.414
Spike2.5	0.639	0.226	0.313	1.3	0.034	0.129	0.554
Blank6		0.123	0.028	1.97	0.017	0.037	0.016
Spike1.6	0.407	0.171	0.177	1.04	0.026	0.083	0.36
Spike2.6	0.567	0.196	0.253	1.03	0.029	0.11	0.492
Blank7		0.096	0.022	1.47	0.017	0.029	0.019
Spike1.7	0.311	0.14	0.148	1.44	0.024	0.075	0.318
Spike2.7	0.522	0.163	0.207	0.894	0.024	0.093	0.416

Blank(ug)	0	36.94	9.5	409	3.24	9.98	3.96
Spike1(ug)	304.42	409.9	399.22	422.12	368.12	360.16	220.96
Spike2(ug)	273.78	428.36	401.26	294.84	381.6	374.4	191.1
Theoretic	60.884	74.592	77.944	2.624	72.976	70.036	43.4
aly %	54.756	78.284	78.352	-22.832	75.672	72.884	37.428